

Needs Tailored Interoperable Railway Infrastructure

# Corrugation

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# Task 2.4: Life extension for plain line through preventing corrugation



To provide a better understanding of corrugation and what can be done to prevent it.

- Experimental tests conducted in the Turkish railways include: 1)
   a catalogue of corrugation and track parameters, and 2)
   experiments on corrugated rail making use of three fastening
   systems available from the industry.
- A further analysis of the 3D FE modelling approach and new insights about short pitch corrugation. The global explanation of the dynamic conditions and the resulting corrugation damage are described. The modelling approach is not able yet to develop corrugation from smooth rail condition.





#### Corrugation catalogue

#### **Corrugation Section:**

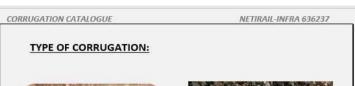
- Wavelength, Amplitude
- Type of Corrugation

#### Track parameters:

- Type of Rail, Rail Grade, Sleepers, Fastening Rail Pad
- Curvature (Straight / Curve), Lubrication
   Condition, Date of Renewal/ Reparation

#### Traffic

- Type of Traffic, Single/ Double Traffic Direction
- Axle Load of Passenger Trains, Freight Trains
- Speed Limit for Passenger Trains, Freight Trains
- Vehicle Velocity, Vehicle in Acceleration, Vehicle in Deceleration
- Number of Daily Passenger Trains, Number of Freight Trains, Gross Ton (Annually)







Wavelength	100-300mm
Amplitude	25µm
Type of Corrugation	Medium Pitch
TRACK P.	ARAMETERS
Type of Rail	UIC 60 E
Rail Grade	900
Type of Sleepers	B70 Concrete
Type of Fastening Syster	n Skl 14
Type of Rail Pad	RP 700
Curvature (Straight/Curv	ve) Straight
ubrication Condition	Unavailable

TRAFFIC		
Type of Traffic	Mixed Traffic	
Single/ Double Traffic	Double Traffic	
Direction Axle Load of Passenger Trains	Condition 12 tonnes	
Axle Load of Freight Trains	22.5 tonnes	
Speed Limit for Passenger Trains	100 km/h	
Speed Limit for Freight Trains	70 km/h	
Vehicle Velocity	120 km/h	
Vehicle in Acceleration	35 km/h	
Vehicle in Deceleration	30 km/h	
Number of Daily Passenger Trains	6 Passenger Trains	
Number of Freight Trains	8 Freight Trains	
Gross Ton (Annually)	4.450.000 gtp	

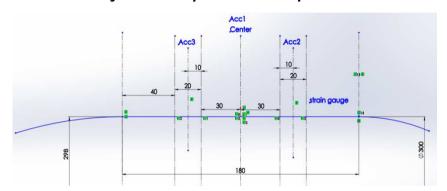
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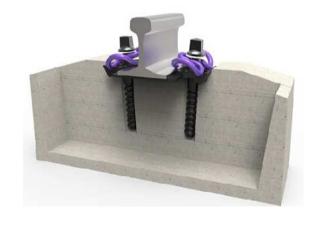


Eskişehir- Afyon- Kütahya Line











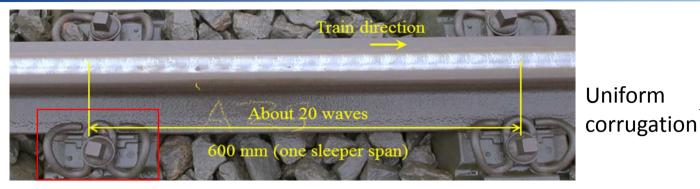
# Modelling part:



- Background
- Model and method
- Conclusions and further research
- Questions

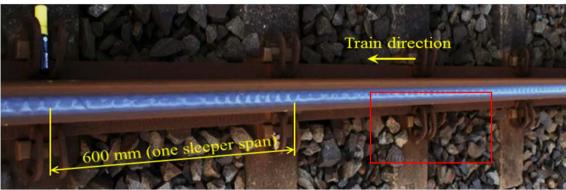
## 1 Background



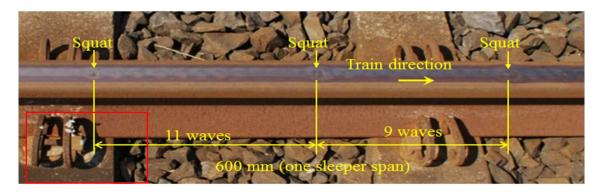


Uniform amplitude

wavelength



Corrugation variations in wavelength and amplitude

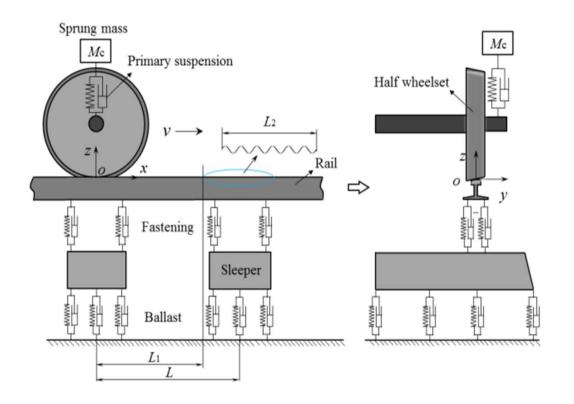


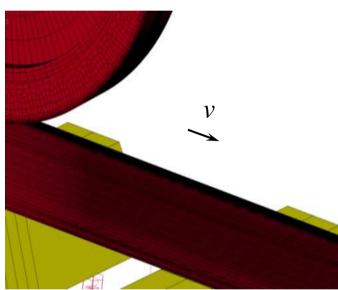
Corrugation variation in amplitude and corrugation induced squats

### 2 Model and methods









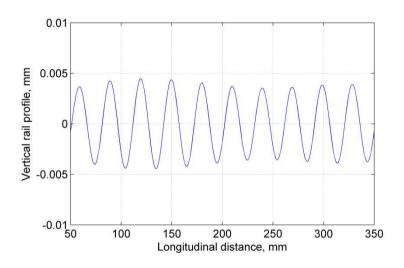
Schematic diagram of the model Parameters from typical Dutch network

FE model in 3D

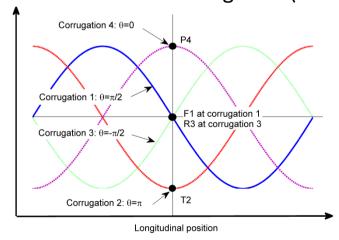








#### Field measurement of corrugation (~30 mm)



4 positions to be investigated

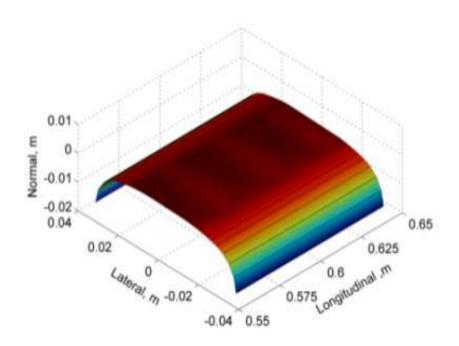
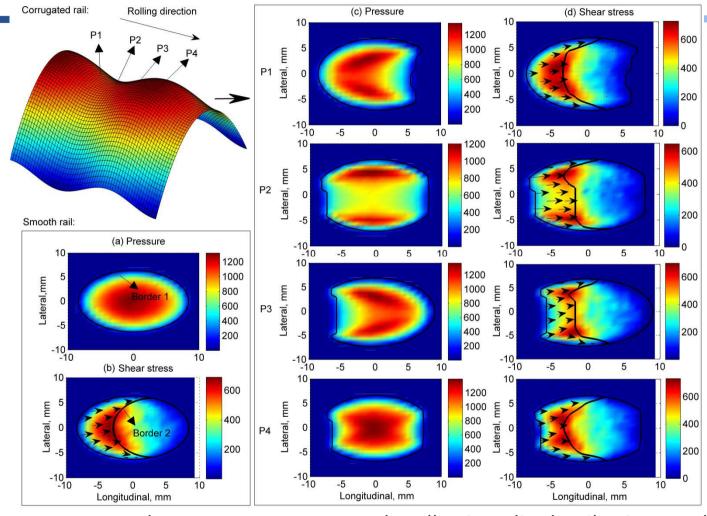


Illustration of the applied corrugation (corrugation 2 with P2 at 0.6 m, only 3 complete waves are plotted).









Contact pressure, shear stress, contact patch, adhesion-slip distributions and vector graphs of micro-slips when A = 20  $\mu$ m (projection onto the xOy plane; Border 1: contact patch border; Border 2: adhesion-slip distribution border).

### 3 Contact solutions



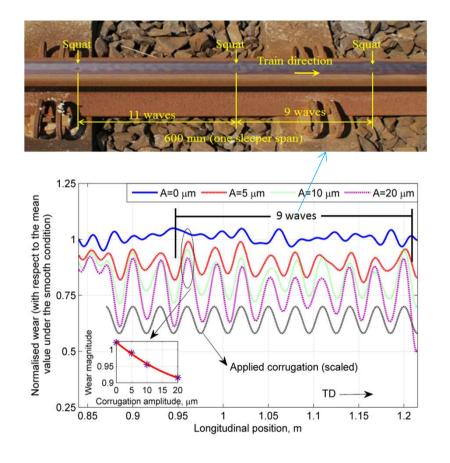
#### Summary:

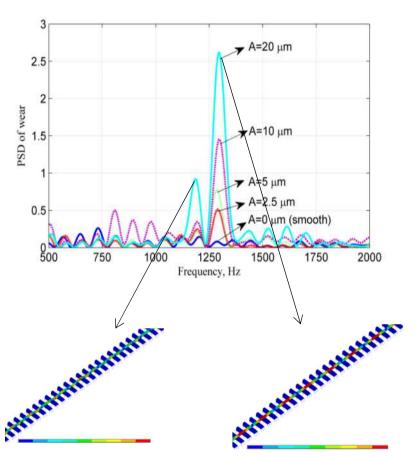
With increases in the corrugation amplitude:

- The increases in the contact area, maximum pressure, shear stress and micro-slips at the corrugation crest are small, and some of them even decrease.
- Changes at the trough are large. The large micro-slip and the significantly reduced contact pressure at the trough are the major contributions to the differential wear, which causes corrugation initiation and growth.

### 4 Other results: differential wear







Differential wear in-phase with corrugation

Vertical track mode

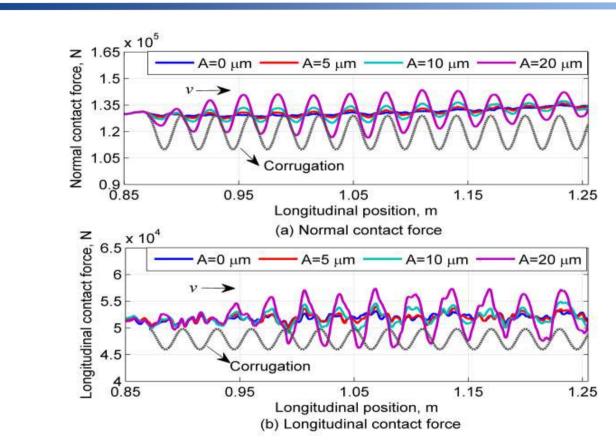
Longitudinal track mode

Becoming dominant when corrugation is severe.

For corrugation initiation





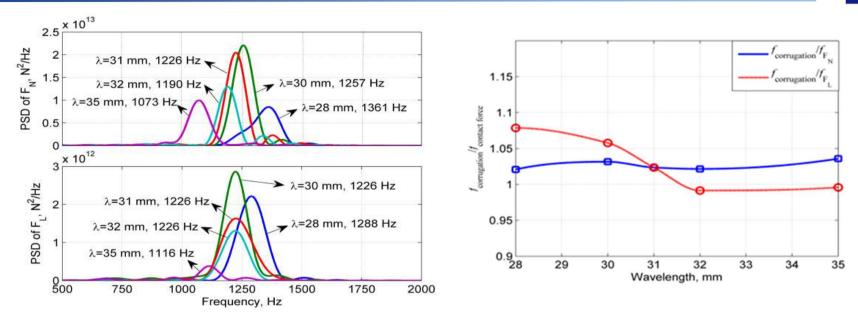


Contact forces are not in consistent with the corrugation.

Dynamic wheel-rail contact forces obtained for the corrugation







- (a) PSD of FN (upper) and FL (lower)
- (b) Ratio of corrugation over contact force frequency
- 1. The frequencies of the normal (FN) and longitudinal (FL) forces are different from the corrugation excitation frequency;
- 2. Their frequencies are varied with corrugation wavelength, at around 31 mm they converge to the same frequency;
- 3. The longitudinal contact frequency is less influenced by the corrugation than the vertical contact force.

### 5 Conclusions and further work



- In the presence of corrugation, contact patch, stresses and micro-slip distributions will be re-distributed.
- Wear, under an applied corrugation, is in-phase with the corrugation and the corrugation will not grow.
- Besides the generally accepted hypothesis that vertical vibration for corrugation, longitudinal modes are more important for the initiation of corrugation.

### 5 Conclusions and further work



- The frequencies of the vertical and longitudinal vibration modes and contact forces as well as the resulting wear are different.
- Therefore, they should be consistent with the corrugation for initiation and growth.
- The results explain the occurrence of rail squats induced by the corrugation.
- Further work: to investigate the track parameters and reproduce the consistent corrugation initiation and growth.

# Questions



Thank you for your attention!